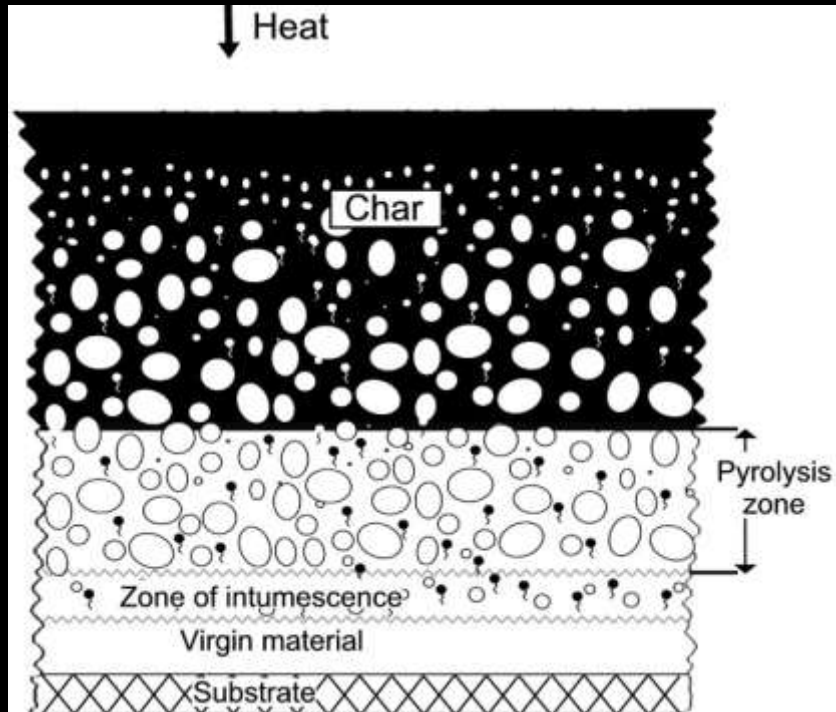


How to protect aircraft against fire with an intumescent cake?

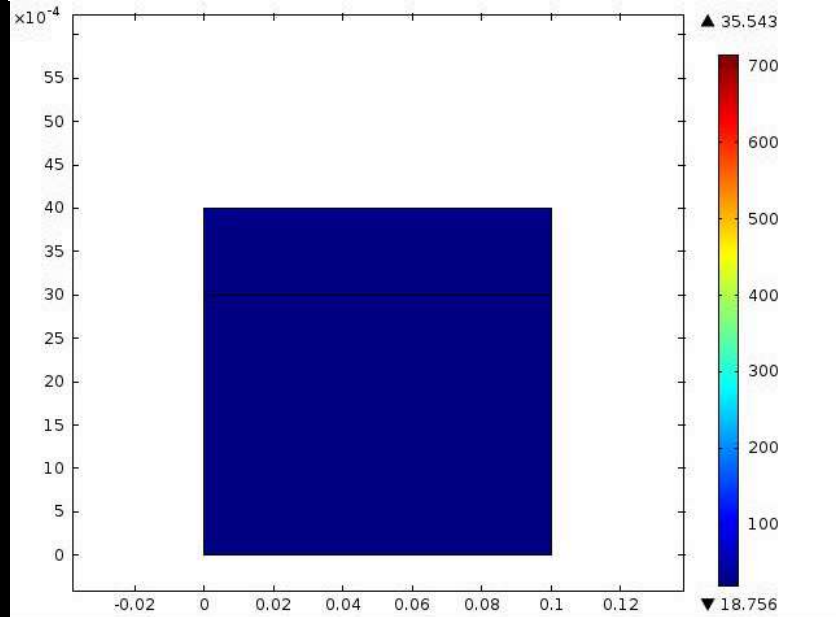
Serge BOURBIGOT

R₂FIRE@UMET-UMR/CNRS 8207

Intumescence?



**Expanding char
forming heat and
mass barrier**

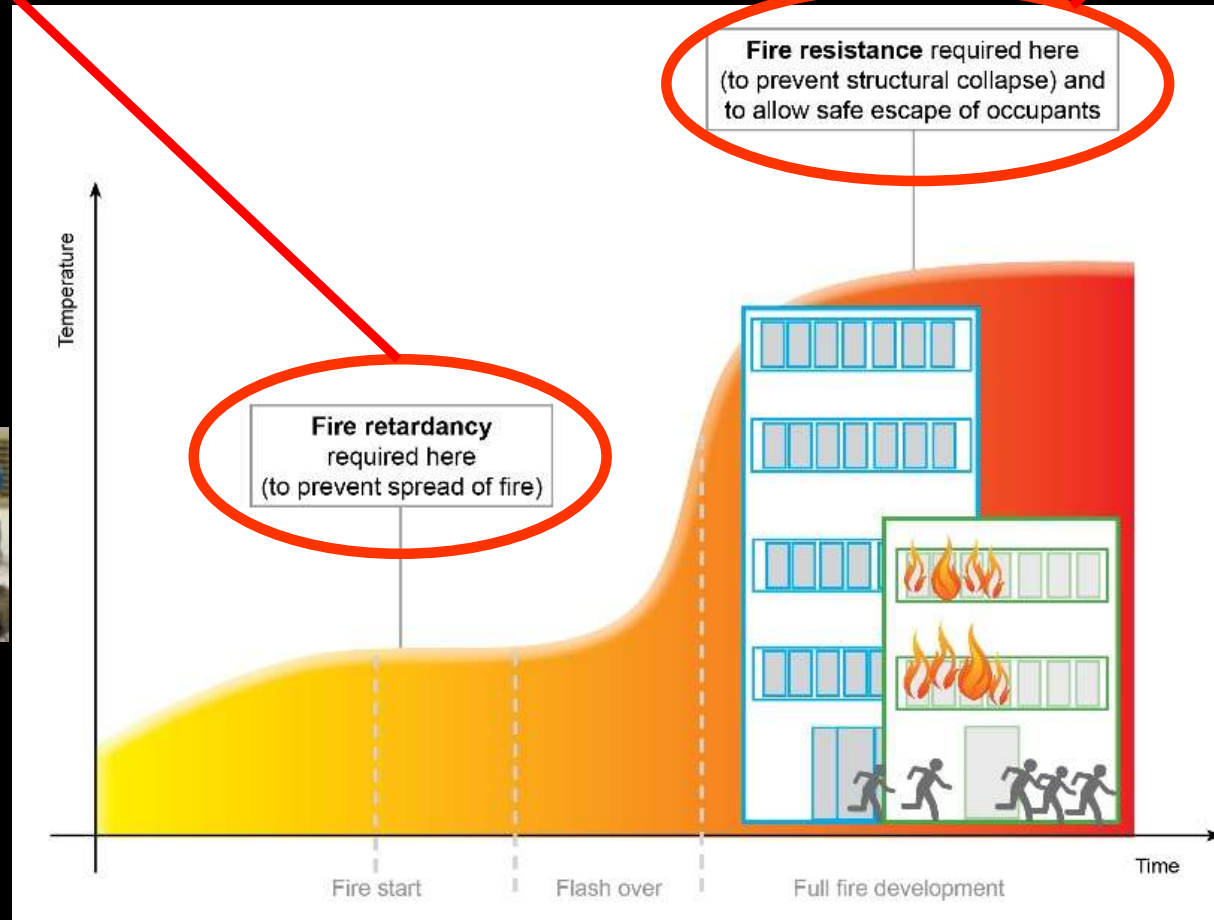


Intumescence for reaction and resistance to fire

- ▷ **Applications:** E&E, railway, cable & wire, aircraft cabin ...
- ▷ **Fire scenarios (testing):** UL94, glow wire, cone calorimeter, SBI, EN 50399 ...



- ▷ **Applications:** building, offshore platform, aircraft ...
- ▷ **Fire scenarios:** UL1709, ISO834, ISO2685, jetfire ...



Fire protection of CFRP





Fire resistance of fuselage and other parts of aircraft: **full scale test or burnthrough test (jet fuel fire at ~186 kW/m²)**



Post-crash fire simulation in full scale indoor at FAA

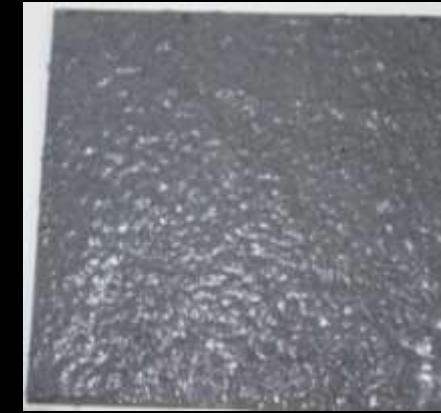


- ❑ Time consuming
- ❑ Expensive
- ❑ Slow development



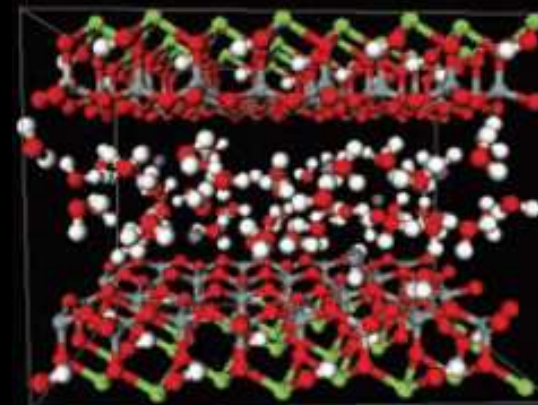
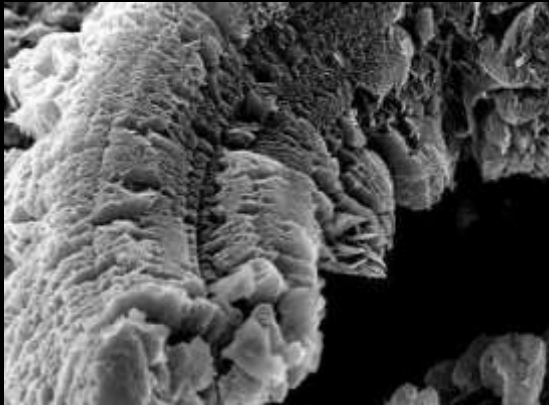
Burnthrough test (NexGen)

Silicone-based intumescent coating



Intumescent paint on CFRP: silicone-based coating containing expandable graphite* compared to low intumescenting paint

Silicone formulation	F1 – High intumescenting coating*	F2- Low intumescenting coating
Silicone matrix	56%	56%
Expandable graphite	25%	-
Calcium carbonate	12%	37%
Clay	7%	7%

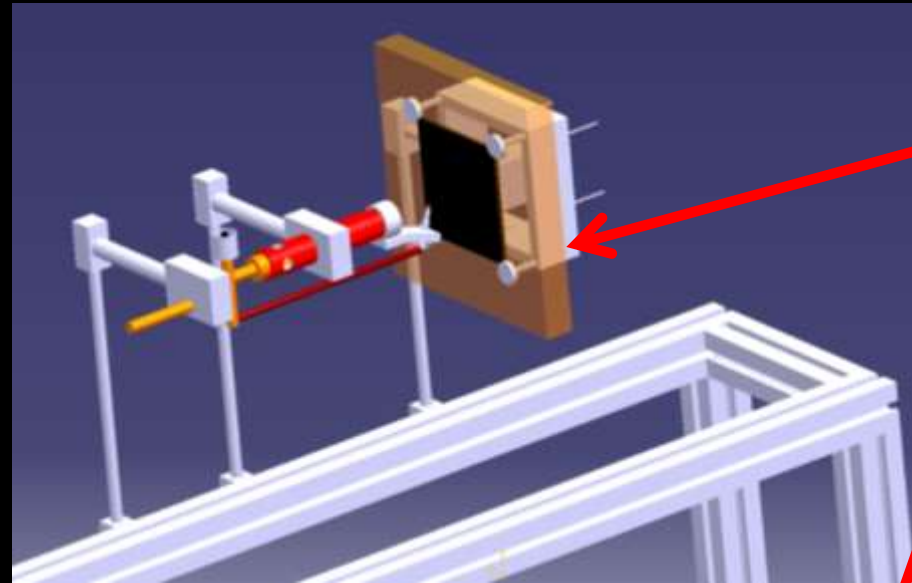


*S. Bourbigot et al. "Protecting substrates against damages by fire", WO 2013/150121 - Dow Corning, 2013



Small scale test: Experimental set up

Infrared
pyrometer and
Th. stuck on
composite ($T = f(t)$)

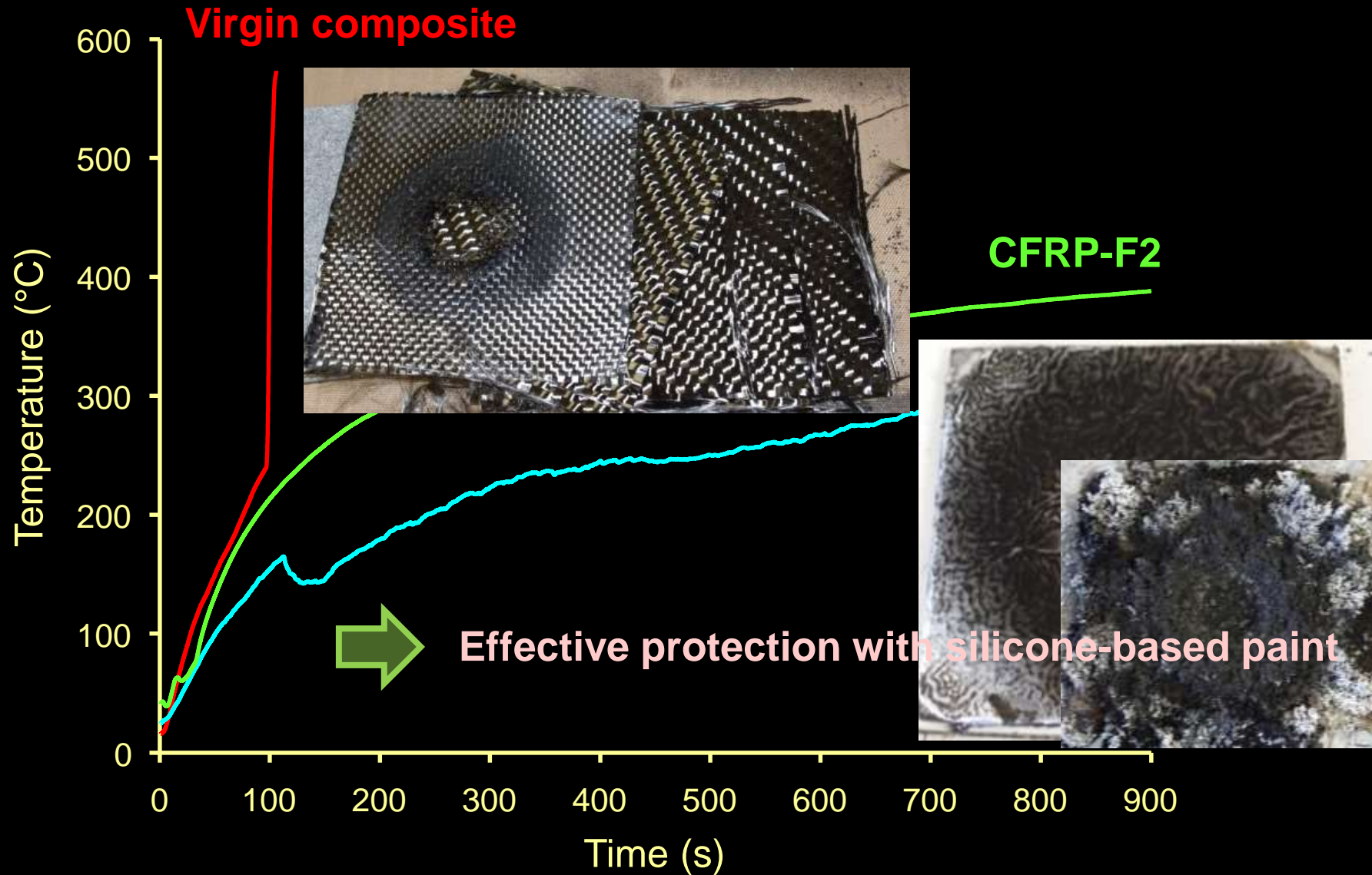


Sample +
holder
(insulative
ceramic)

Burner (200
 kW/m^2 at the
surface –
 $T_{\text{flame}} \sim 1100^\circ\text{C}$)



Protection by intumescence: 1000 μm



Protection by intumescence



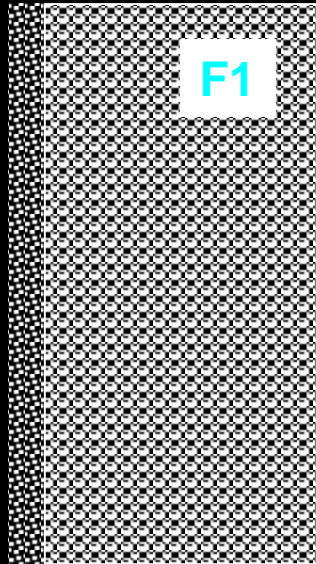
Virgin composite



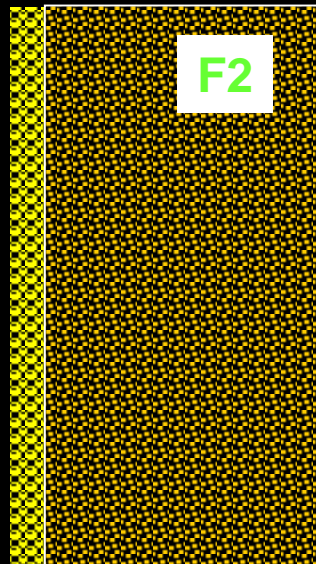
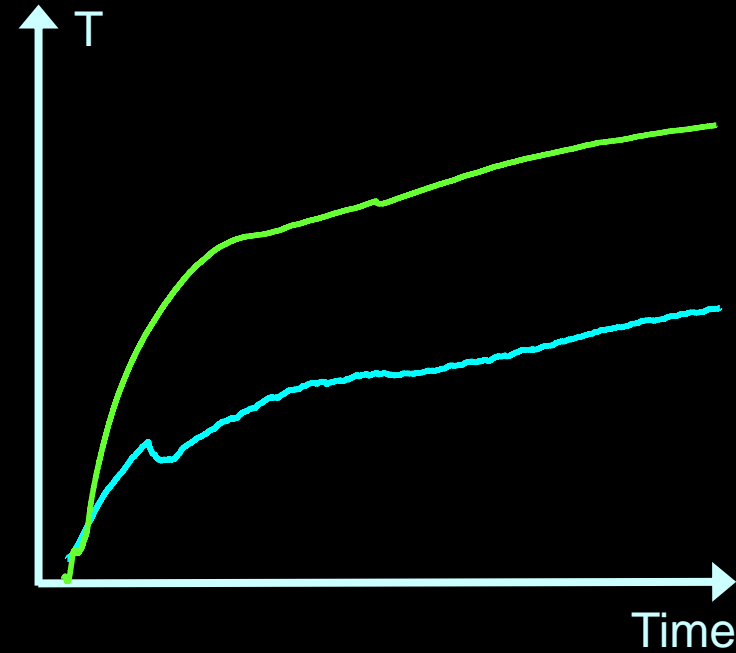
CFRP-F1



Mechanism of protection



- Heat barrier: high expansion, low k ($0.4 \text{ W/m.K@600}^\circ\text{C}$)
- Structure: high cohesion thanks to chemical interactions (SiC, Ca-Si)



- Heat barrier: low expansion, low k ($0.4 \text{ W/m.K@600}^\circ\text{C}$)
- Structure: cohesive porous structure (highly polymerized Si, Ca-Si)

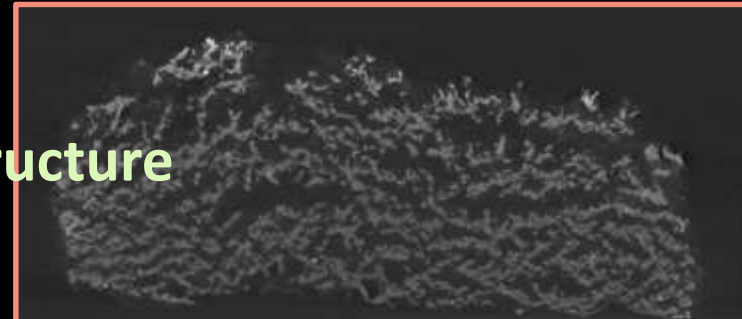
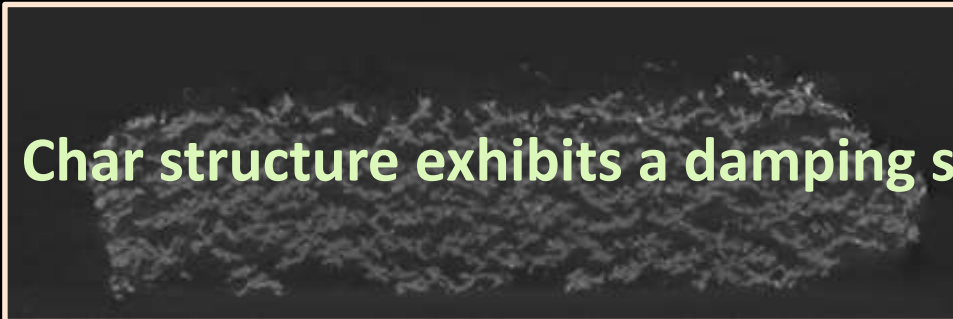
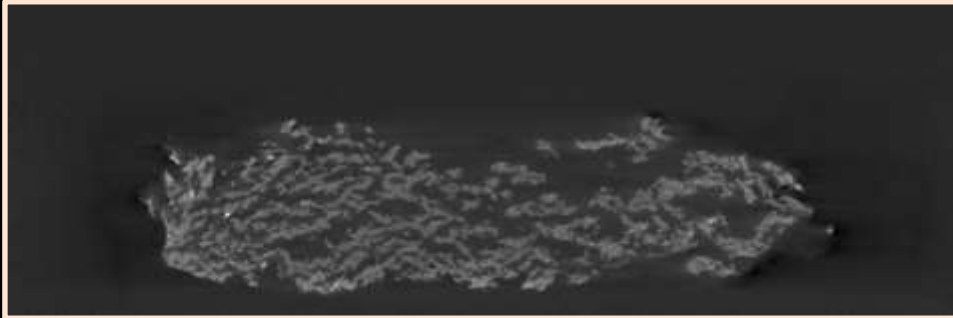
Char characterization: X-ray tomography



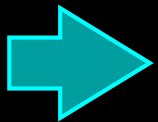
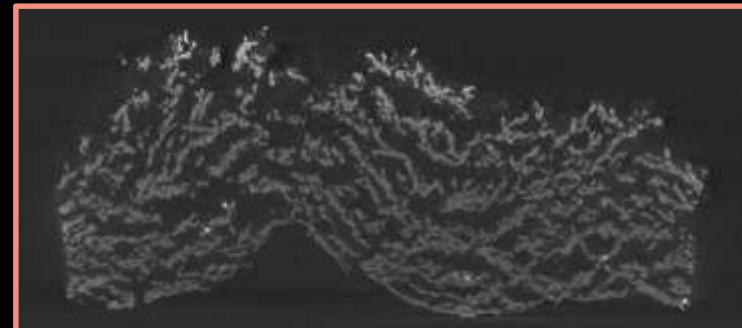
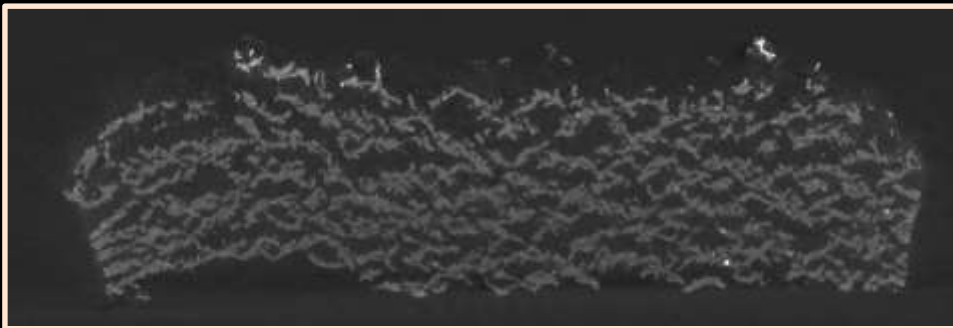
Internal intumescent structure : slices at different z of char residues after test

After intumescence

End



Char structure exhibits a damping structure

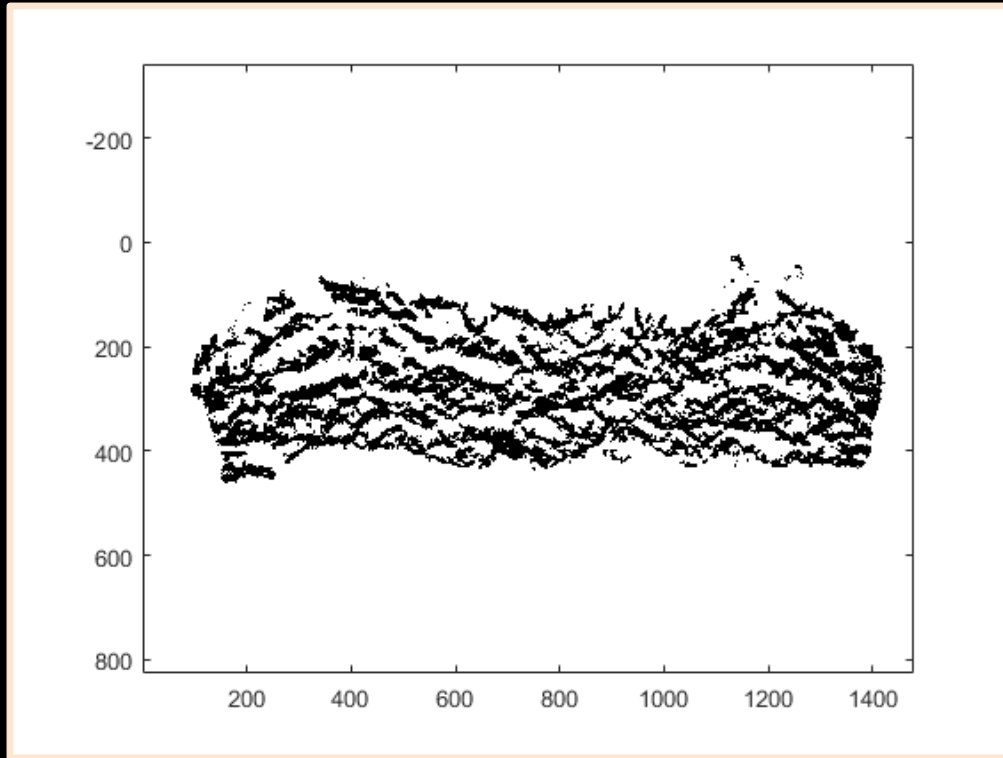


Char characterization: fractal dimension



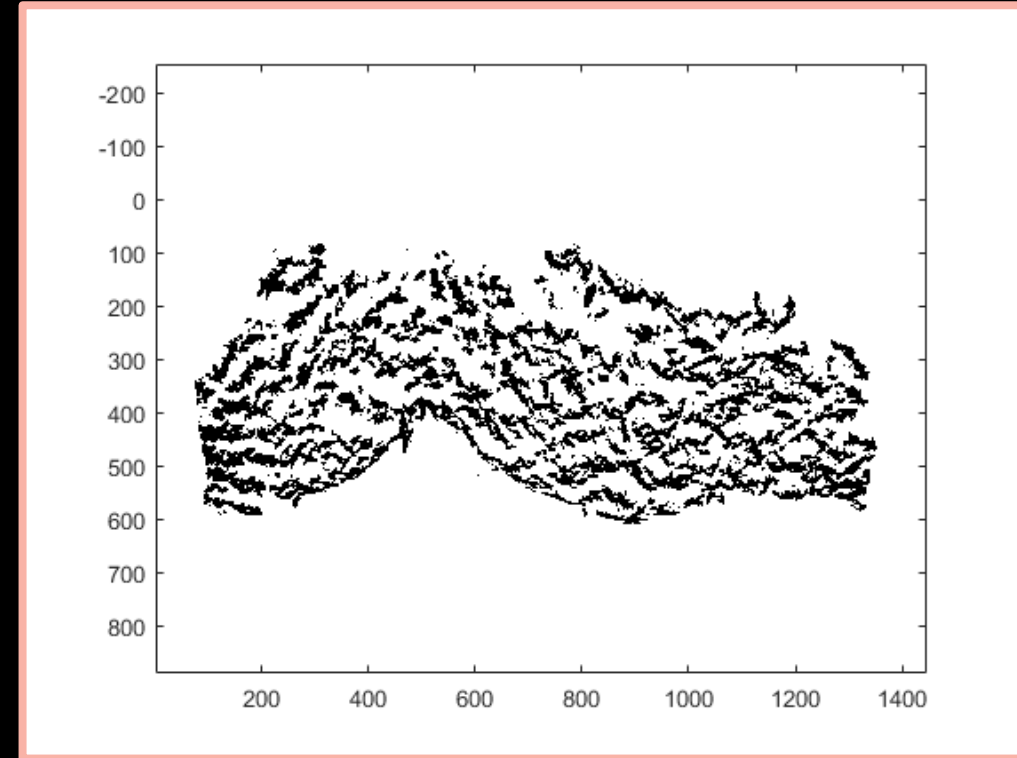
Binarization: extraction of the fractal dimension on a determined scale

After intumescence

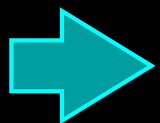


$D_f = 1.7$ on 100-2000 μm

End

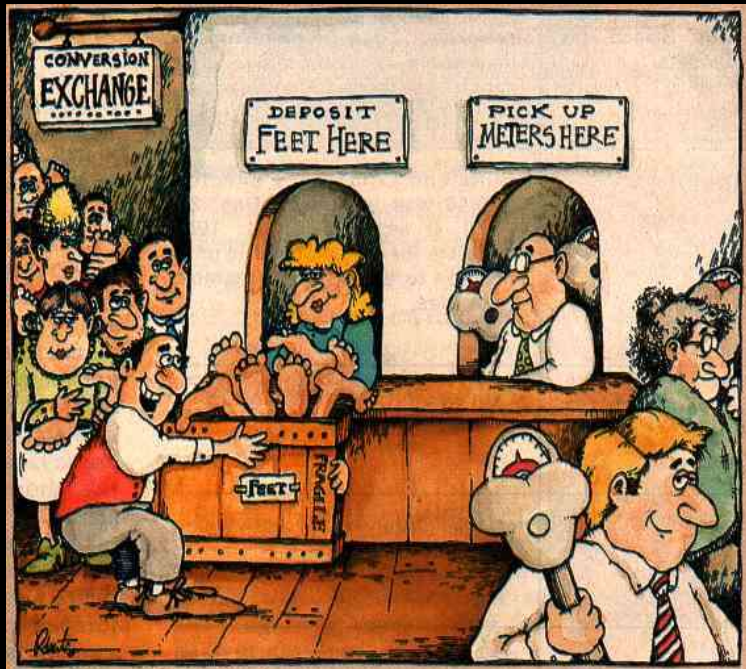


$D_f = 1.7$ on 100-700 μm



D_f suggests an oriented materials (higher aspect ratio):
correlation with char strength?

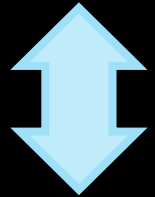
ISO 2685 at reduced scale: dimensional analysis



Fire scenario at the small scale: how to play?



Lezard as big
as a house?!



Linear extrapolation: feeling of
visuals!

Toward scale
reduction?



ISO 2685: goal and test



Pass/fail test for equipment located in fire zone
(engine, auxiliary unit):

- Heat flux of 116 kW/m²
- T_{flame} of 1100°C
- Withstanding of the component for 5 min ⇒ fire proof
- Withstanding of the component for 15 min ⇒ fire resistant



$$\begin{cases} \rho C \dot{T} - k \Delta \bar{T} = \frac{q_{av} - q_{ar}}{e_p} \\ q_{ar} = h_{ar}(T - T_{amb}) + \varepsilon \sigma (T^4 - T_{amb}^4) \\ q_{av} = h_{av}(x, y)(T_g - T) + C(x, y) \sigma (T_f^4 - T^4) - \varepsilon \sigma (T^4 - T_{amb}^4) \end{cases}$$

➔ **Dimensionless numbers are determined:**

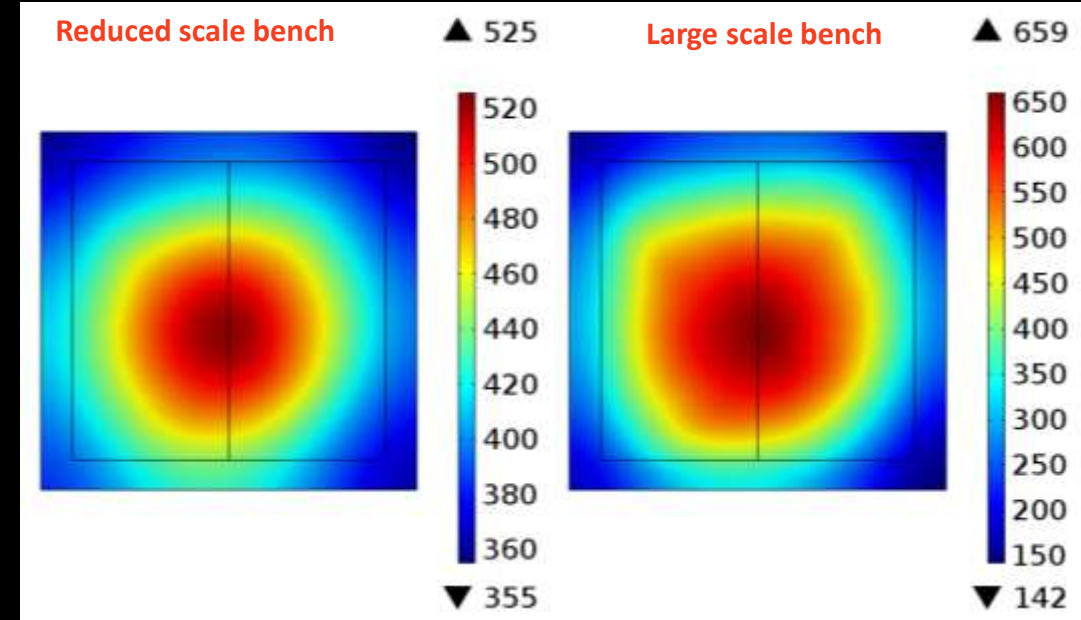
$\tilde{x} = x/L$ $\tilde{y} = y/L$ $\tilde{t} = t/\tau$ $\tilde{T} = T/T_{amb}$

τ : duration of the experiment
 L : length of the plate

$$\frac{\tau e_p}{\tau} \frac{\partial \tilde{T}}{\partial \tilde{t}} - \left(\frac{e_p}{L}\right)^2 \Delta \tilde{T} = B_i^{av} \left(\frac{T_g}{T_{amb}} - \tilde{T}\right) + CN_r \left(\left(\frac{T_f}{T_{amb}}\right)^4 - \tilde{T}^4\right) - 2\varepsilon N_r (\tilde{T}^4 - 1) - B_i^{ar} (\tilde{T}^4 - 1)$$

$$B_i^{av} = \frac{e_p h_{av}}{k} \quad B_i^{ar} = \frac{e_p h_{ar}}{k} \quad \rightarrow \text{Biot numbers linked to the convection on the 2 faces}$$

$$F_o^{ep} = \tau / \tau_{ep} \quad \tau_{ep} = \frac{\rho C_p e_p^2}{k} \quad N_r = \frac{e_p \sigma T_{amb}^3}{k} \quad \rightarrow \text{Fourier, time and radiative numbers}$$



➔ **Lower temperature field for the small-scale bench**

➔ **No linear extrapolation but dimensional analysis to understand the differences**



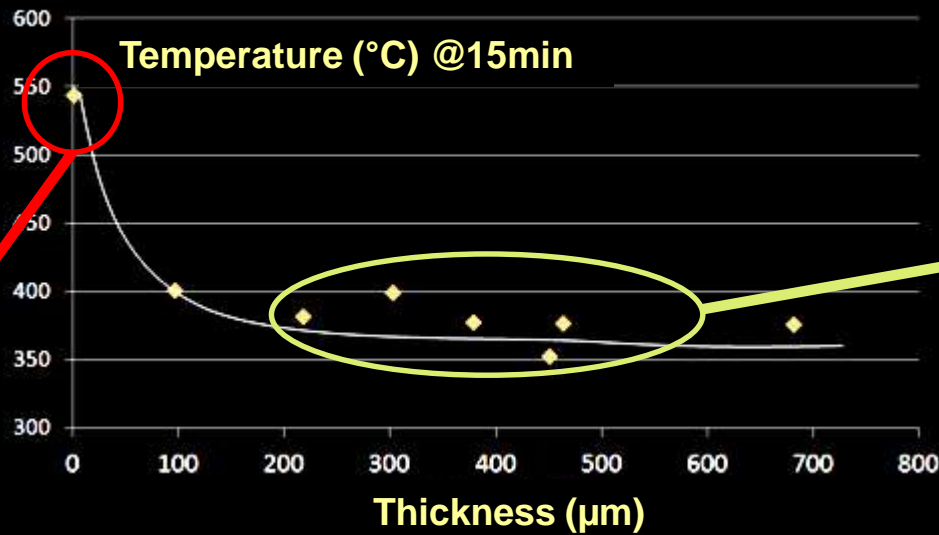
Safran Project:

Design and improvement of a test bench to fire a reduced scale

Small scale test: intumescent CFRP



Evaluation of
intumescent
CFRP

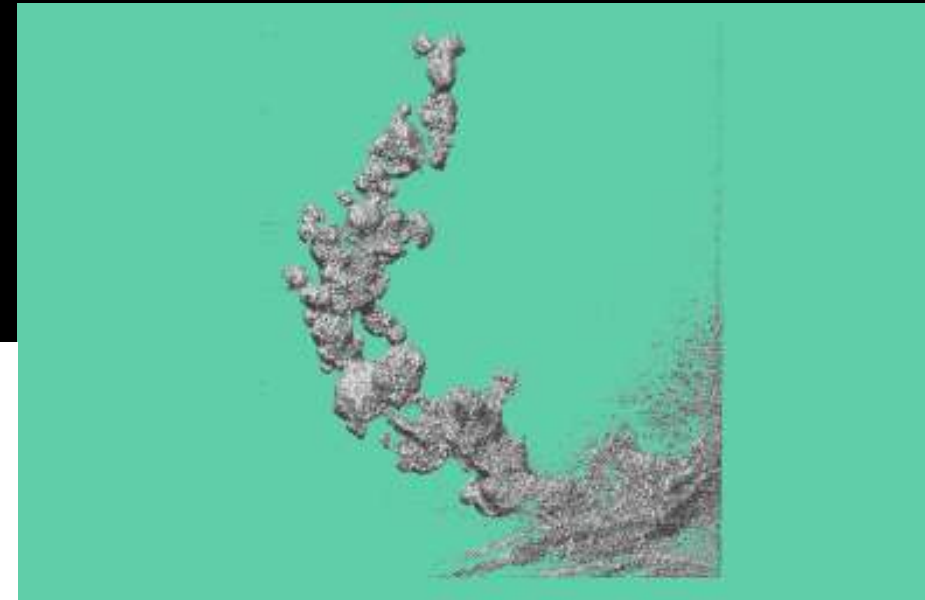


Efficiency of the fire protection
from 250 µm via an
intumescent behavior



Summary and future work

- **Similitude:** *scale reduction is not straight forward but correlation can be found (ISO2685, NexGen...)*
- **Intumescence:** *appropriate way for reaction and resistance to fire*
- **Further models:** *development of model working in flaming conditions (in progress)*
- **Gas phase:** *full characterization of the gas phase taking into account soot (radiative properties)*



Acknowledgment



ERC AdG:
FireBar-
Concept

